

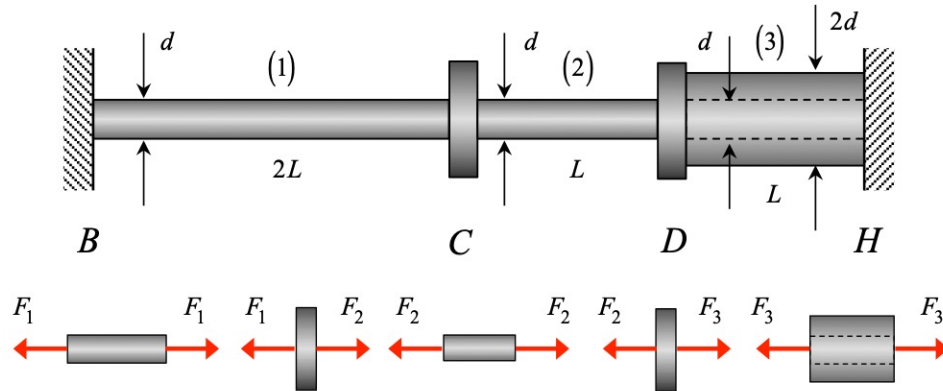
PROBLEM #1 (25 Points):**SOLUTION**

A rod is made up of elastic members (1), (2) and (3), with the material makeup of each member having a Young's modulus of E and a coefficient of thermal expansion of α . Members (1), (2) and (3) have lengths of $2L$, L and L , respectively. Members (1) and (2) have solid cross-sections with a diameter of d , whereas member (3) has a tubular cross-section with inner and outer diameters of d and $2d$, respectively. With the members being initially unstressed, the temperatures of (1) and (2) are increased by amounts of $2\Delta T$ and ΔT , respectively, while the temperature of (3) is held constant.

As a result of the temperature changes described above:

- Determine the axial load (force) carried by each member. State whether each member is experiencing a compressive or tensile load.
- Determine the axial strain in each member. Include an appropriate sign with each strain.

Leave your answers in terms of, at most, E , α , L , d and ΔT .

**1. Equilibrium**

$$(1) \text{ (C): } \sum F = -F_1 + F_2 = 0 \Rightarrow F_1 = F_2$$

$$(2) \text{ (D): } \sum F = -F_2 + F_3 = 0 \Rightarrow F_3 = F_2$$

2. Force/elongation

$$(3) \quad e_1 = \frac{F_1(2L)}{EA_1} + \alpha(2\Delta T)(2L) \quad ; \quad A_1 = \pi \left(\frac{d}{2} \right)^2$$

$$(4) \quad e_2 = \frac{F_2 L}{EA_2} + \alpha \Delta T L \quad ; \quad A_2 = \pi \left(\frac{d}{2} \right)^2$$

$$(5) \quad e_3 = \frac{F_3 L}{EA_3} \quad ; \quad A_3 = \pi \left(\frac{2d}{2} \right)^2 - \pi \left(\frac{d}{2} \right)^2 = \frac{3}{4} \pi d^2$$

3. Compatibility

$$u_C = u_B + e_1 = e_1$$

$$u_D = u_C + e_2 = e_1 + e_2$$

$$(6) \quad u_H = u_D + e_3 = e_1 + e_2 + e_3 = 0$$

4. Solve

$$(3)-(6) \Rightarrow 2 \frac{F_1 L}{E \pi (d^2/4)} + 4 \alpha \Delta T L + \frac{F_2 L}{E (d^2/4)} + \alpha \Delta T L + \frac{F_3 L}{E (3d^2/4)} = 0 \Rightarrow$$
$$8 \frac{F_1}{E \pi d^2} + 5 \alpha \Delta T L + 4 \frac{F_2}{E d^2} + \frac{4}{3} \frac{F_3}{E d^2} = 0 \Rightarrow$$
$$8F_1 + 4F_2 + \frac{4}{3}F_3 = -5\pi\alpha\Delta T L E d^2$$

Combining with (1) gives:

$$\left(8 + 4 + \frac{4}{3}\right) F_1 = -5\pi\alpha\Delta T L E d^2 \Rightarrow F_1 = F_2 = F_3 = -\frac{3}{8}\pi\alpha\Delta T L E d^2 \text{ (compression)}$$

Strains

$$\varepsilon_1 = \frac{e_1}{2L} = \frac{4F_1}{E\pi d^2} + 2\alpha\Delta T = \frac{4F_1}{E\pi d^2} \left(-\frac{3}{8}\pi\alpha\Delta T L E d^2\right) + 2\alpha\Delta T = \frac{1}{2}\alpha\Delta T$$
$$\varepsilon_2 = \frac{e_2}{L} = \frac{4F_2}{E\pi d^2} + \alpha\Delta T = \frac{4}{E\pi d^2} \left(-\frac{3}{8}\pi\alpha\Delta T L E d^2\right) + \alpha\Delta T = -\frac{1}{2}\alpha\Delta T$$
$$\varepsilon_3 = \frac{e_3}{L} = \frac{4F_3}{3E\pi d^2} = \frac{4}{3E\pi d^2} \left(-\frac{3}{8}\pi\alpha\Delta T L E d^2\right) = -\frac{1}{2}\alpha\Delta T$$

Name (Print) SOLUTION
(Last) (First)

PROBLEM # 2 (25 points)

The critical components for the design of the planar truss in Figure 2a are considered to be member AB and the pin at C (shown in Figure 2b). The truss is subjected to a single downward force P at A. All members of the truss have a cross-sectional area of $A=1 \text{ in}^2$. The cross-sectional area of the pin at C is $A_C=0.5 \text{ in}^2$. The factor of safety (FS) against failure of AB by yielding is $FS_{AB}=3$. The factor of safety against ultimate shear failure of the double-sided pin at C is $FS_C=4$.

For member AB, $\sigma_Y=36 \text{ ksi}$ and for the pin material $\tau_U=48 \text{ ksi}$.

Find the largest P that can be applied without failure of the member AB and pin C.

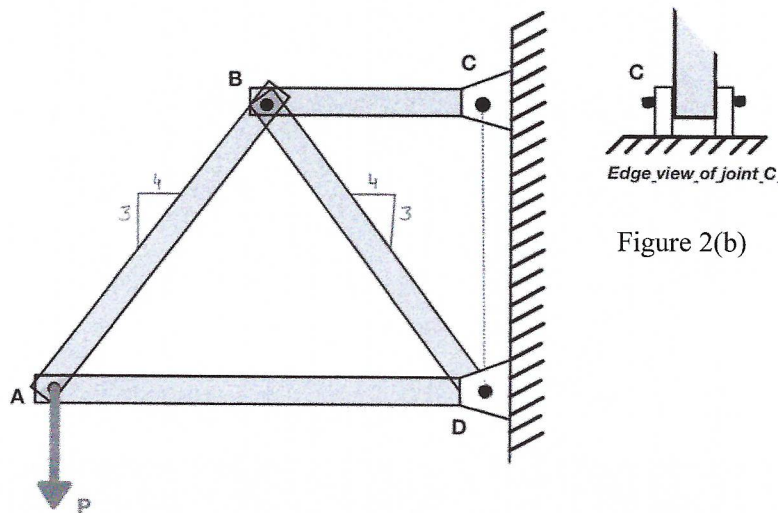
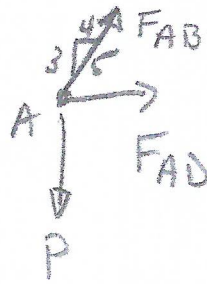


Figure 2(a)

Figure 2(b)

PROBLEM #2

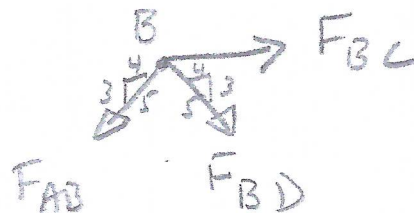
Pin A



$$\sum F_y = \frac{3}{5} F_{AB} - P = 0$$

$$F_{AB} = \frac{5P}{3}$$

Pin B



$$\sum F_x = F_{BC} + \frac{4}{5} F_{BD} - \frac{4}{5} F_{AB} = 0$$

$$\sum F_y = -\frac{3}{5} F_{AB} - \frac{3}{5} F_{BD} = 0$$

$$F_{BD} = -F_{AB} = -\frac{5P}{3}$$

$$F_{BC} = \frac{4}{5} F_{AB} - \frac{4}{5} F_{BD}$$

$$= \frac{4}{5} \left[\frac{5P}{3} \right] - \frac{4}{5} \left[-\frac{5P}{3} \right]$$

$$F_{BC} = \frac{8}{3} P$$

For AB

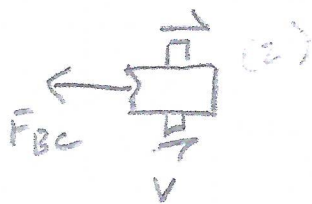
$$\sigma_{AB} = \frac{F_{AB}}{A} = \boxed{\frac{5P}{3} = \tau_{AB}}$$

$$(FS)_{AB} = \frac{\sigma_y}{\sigma_{AB}} = 3 \Rightarrow \sigma_{AB} = \frac{\sigma_y}{3}$$

$$\boxed{\frac{5P}{3} = \frac{36 \text{ ksi}}{3} = 12 \text{ ksi}}$$

$$\boxed{P_{AB} = \frac{3}{5} (12) = 7200 \text{ lb.}} = \frac{36}{5}$$

For pin c



$$V_{pin} = \frac{F_{Bc}}{2} = \frac{8}{(3)(2)} P$$

$$V_{pin} = \frac{4}{3} P$$

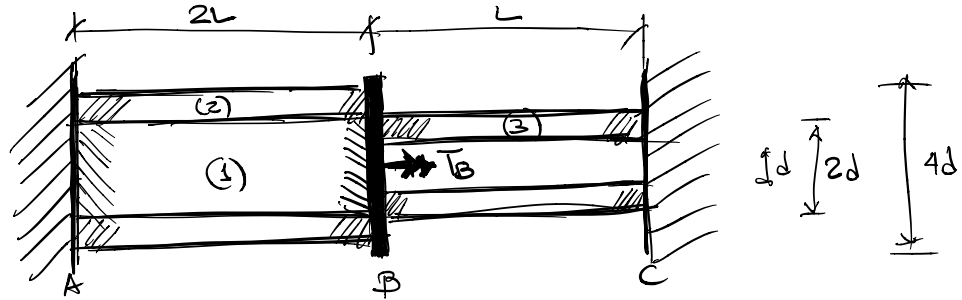
$$\tau_{pin} = \frac{V_{pin}}{A_p} = \frac{\frac{4}{3} P}{0.5} = \boxed{\frac{8}{3} P = \tau_{pin}}$$

$$(FS)_{pin} = \frac{\tau_u}{\tau_{pin}} \Rightarrow \tau_{pin} = \frac{\tau_u}{(FS)_{pin}} = \frac{48}{4} = 12 \text{ ksi}$$

$$\frac{8}{3} P = 12 \text{ ksi} \quad (1) \quad \boxed{P_{pin} = \frac{36 \text{ ksi}}{8} = 4,500 \text{ lb}}$$

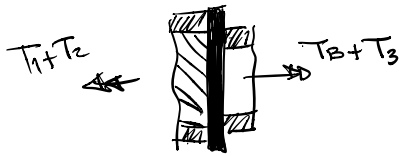
$$\boxed{P_{allow} = 4,500 \text{ lb}}$$

Smallest



• FBD & Equilibrium

→ 1 equation & 3 unknowns
STATICALLY INDETERMINATE



$$T_B + T_3 - T_1 - T_2 = 0 \quad (*)3$$

• Compatibility conditions

• Torque-twist behavior

$$\phi_A = 0 \quad \& \quad \phi_C = 0$$

$$\left. \begin{aligned} \phi_1 &= \phi_B \\ \phi_2 &= \phi_B \\ \phi_3 &= -\phi_B \end{aligned} \right\} \begin{aligned} \phi_1 &= \phi_2 \\ \phi_2 &= -\phi_3 \end{aligned}$$

⇒ ⇒

$$T_1 \frac{L_1}{G_1 I_{p1}} = T_2 \frac{L_1}{G_2 I_{p2}} \quad (*)1$$

$$T_2 \frac{L_1}{G_2 I_{p2}} = -T_3 \frac{L_3}{G_3 I_{p3}} \quad (*)2$$

with ... $I_{p1} = \frac{\pi (2d/2)^4}{2} = \frac{\pi d^4}{2}$

$$I_{p2} = \frac{\pi}{2} [(4d/2)^4 - (2d/2)^4] = \frac{\pi}{2} [16d^4 - d^4] = \frac{\pi}{2} 15d^4$$

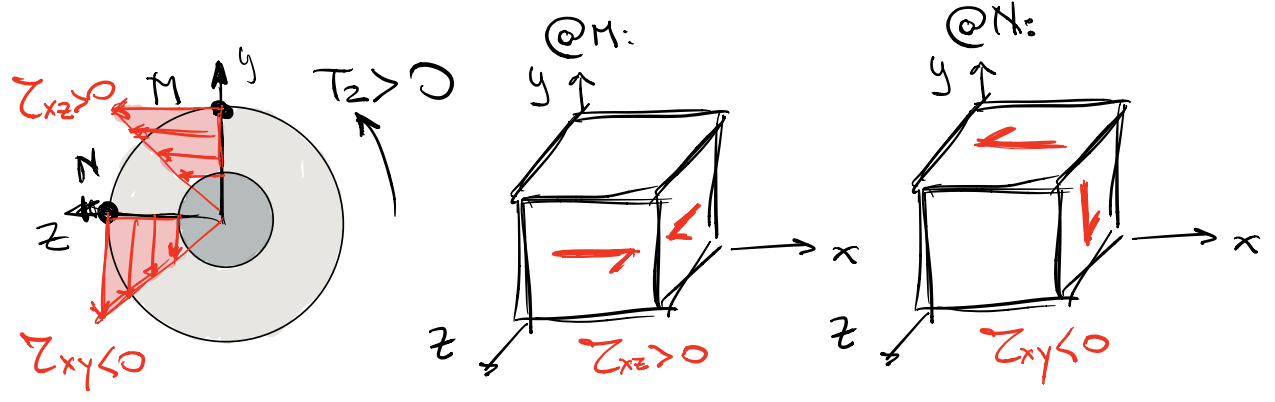
$$I_{p3} = \frac{\pi}{2} [(2d/2)^4 - (d/2)^4] = \frac{\pi}{2} [d^4 - \frac{1}{16}d^4] = \frac{\pi}{32} [16d^4 - d^4] = \frac{\pi}{32} 15d^4$$

• Solve

$$(*)1 \Rightarrow T_1 = T_2 \frac{G_1}{G_2 15}$$

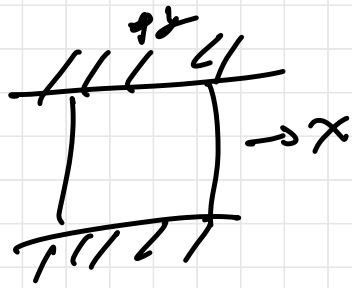
$$(*)2 \Rightarrow T_3 = -T_2 \frac{L_1}{L_3} \frac{G_3}{G_2} \frac{1}{16}$$

$$(*)3 \Rightarrow T_B = T_2 \left[\frac{G_3 L_1}{16 G_2 L_3} + \frac{G_1}{15 G_2} + 1 \right] \Rightarrow \begin{aligned} T_2 &= \frac{1}{3} T_B \\ T_1 &= \frac{1}{3} T_B \\ T_3 &= -\frac{1}{3} T_B \end{aligned}$$



4. Part A

use Generalized
Hooke's law



(c) $\sigma_x = 0$, $\epsilon_x = (1-\nu)\alpha\Delta T$
 $\sigma_y = -\alpha E\Delta T$, $\epsilon_y = 0$

4) Part B

- a) F
- b) T
- c) F
- d) F

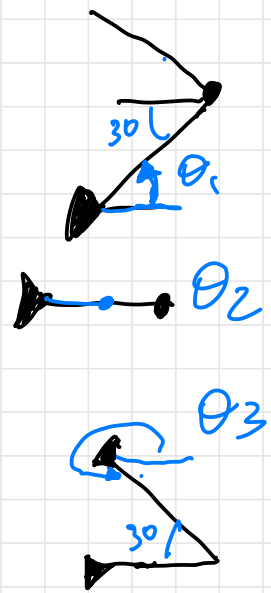
- e) F
- f) F
- g) T

4) Part C

$$\theta_1 = \pi/6$$

$$\theta_2 = 0$$

$$\theta_3 = \frac{\pi}{6}$$

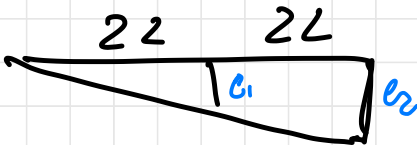


4) Part D

(a) $l_1 = l_2$

(b) $l_1 = -l_2$

(c) $l_1 = l_2/2$



d) $l_1 + l_2 = 0$

e) move the
pivot