

**EE321 Exam 2  
Spring 2010**

Notes: **You must show work for credit.**  
**The last page of exam is blank for extra paper if needed.**

**Good luck, and have a safe and relaxing spring break!**

- 1) 34 pts. Measuring the a-phase impedance looking into a stepper motor, it is found that the inductance varies between 4 mH and 20 mH, and has 8 maxima as it is rotated over one revolution, and that the resistive part of the impedance is constant at 4  $\Omega$ . If the machine is fed from a drive with a 12 V dc source, and neglecting forward semiconductor voltage drops, what is the maximum load torque that can be applied if the machine is to step forward correctly using single step excitation? What is the minimum load torque (i.e. the most negative value of load torque) which can be applied if the machine is to step forward correctly using single step excitation?

$$R_T = 8$$

$$L_A + L_B = 20 \text{ mH}$$

$$L_A - L_B = 4 \text{ mH}$$

$$L_A = 12 \text{ mH} \quad L_B = 8 \text{ mH}$$

$$L_{as}(\theta_r) = 12 + 8 \cos 8\theta_r \text{ mH}$$

$$V_{dc} = 12 \text{ V} \quad r = 4 \Omega$$

$$I_{dc} = \frac{V_{dc}}{r} = \frac{12}{4} = 3 \text{ A}$$

$$T_e = -\frac{1}{2} L_B R_T i_{as}^2 \sin 8\theta_{rm} \quad i_{as} = I_{dc}$$

$$T_e = -\frac{1}{2} \times 8 \times 8 \times 9 \sin 8\theta_{rm} 10^{-3} \text{ Nm}$$

$$T_e = -0.288 \sin 8\theta_{rm} \text{ Nm}$$

$$T_{adv} = \frac{1}{2} T_{e \max} = \frac{1}{2} 0.288 = 0.144 \text{ Nm}$$

Advancement Torque

$$T_{e \min} = T_{e \min} = -0.288 \text{ Nm}$$

- 2) 22 pts. A separately excited dc machine has a armature resistance of 0.2 Ohms, a field resistance of 10 Ohms,  $L_{af}$  of 150 mH. We wish to determine the currents (armature and field) in such a way as to achieve a torque of 2 Nm, while minimizing the loss. What should the armature and field current be? What will the machine loss be at this point? Note: you may assume you are not against any voltage limits.

Resistive losses occur in armature and field resistances

$$\Rightarrow P_{loss} = I_a^2 r_a + I_f^2 r_f$$

for separately excited DC machine

$$T_e = L_{af} I_a I_f \quad \Rightarrow \quad I_a I_f = \frac{T_e}{L_{af}} \quad \text{or} \quad I_f = \frac{T_e}{L_{af} I_a}$$

Rewrite  $P_{loss}$  in terms of  $I_a$  (can also be rewritten in terms of  $I_f$ )

$$P_{loss} = r_a I_a^2 + \left( \frac{T_e}{L_{af} I_a} \right)^2 r_f$$

Minimize loss  $\frac{dP_{loss}}{dI_a} = 0$

$$\frac{dP_{loss}}{dI_a} = 2r_a I_a - 2 \left( \frac{T_e}{L_{af}} \right)^2 \frac{r_f}{I_a^3} = 0$$

$$\Rightarrow I_a^4 = \frac{r_f T_e^2}{r_a L_{af}^2}$$

$$I_a = \left( \frac{r_f T_e^2}{r_a L_{af}^2} \right)^{1/4} = \left( \frac{10}{0.2} \frac{4}{150 \times 10^{-3}} \right)^{1/4} = 9.710 \text{ A}$$

$$\Rightarrow I_f = 1.373 \text{ A}$$

Use these values in  $P_{loss}$  equation

$$P_{loss} = 37.71 \text{ W}$$

- 3.) 22 pts. A permanent magnet dc machine is being fed from a single quadrant chopper, as we discussed in class. The armature resistance is  $100 \text{ m}\Omega$ , and the back emf constant is  $0.2 \text{ Vs}$ , and the armature inductance is  $0.25 \text{ mH}$ . The chopper is supplied from a  $25 \text{ V}$  dc source, has a  $1 \text{ V}$  forward transistor drop, and a  $0.75 \text{ V}$  forward diode drop. At a speed of  $100 \text{ rad/s}$ , the chopper is in discontinuous mode, and has a peak current of  $5 \text{ A}$ . How long is the transistor on? How long does the diode conduct (i.e. what is the duration of non-zero current in the diode within a cycle)?

When transistor is ON the DC machine voltage

equation is

$$V_{dc} = \hat{I}_a r_a + V_{fsw} + L_a \frac{dI_a}{dt} \quad \text{--- (1)}$$

$$\hat{I}_a = \frac{I_{mx}}{2} \quad \& \quad \frac{dI_a}{dt} = \frac{I_{mx}}{T_{on}} + k_v \omega_r$$

from (1)

$$\Rightarrow \frac{I_{mx}}{T_{on}} = \frac{V_{dc} - V_{fsw} - \hat{I}_a r_a - k_v \omega_r}{L_a}$$

$$T_{on} = \frac{L_a I_{mx}}{V_{dc} - V_{fsw} - \hat{I}_a r_a - k_v \omega_r} = \frac{0.25 \times 5 \times 10^{-3}}{3.75} = 0.333 \text{ ms}$$

similarly when transistor is off

$$-\frac{I_{mx}}{t_d} = \frac{-V_d - \hat{I}_a r_a - k_v \omega_r}{L_a}$$

$$\Rightarrow t_d = \frac{I_{mx} L_a}{V_d + \hat{I}_a r_a + k_v \omega_r} = \frac{5 \times 0.25 \times 10^{-3}}{21} = 0.059 \text{ ms}$$

- 4.) 22 pts. A permanent magnet dc machine is supplied by a four-quadrant converter with a hysteresis control. The machine has no armature resistance, and the converter has no forward semiconductor drops (wouldn't it be nice). The desired armature current is  $i_a^*$  and the hysteresis level is denoted  $h$ . When the armature current falls below  $i_a^* - h$ , the converter is switched such that the armature voltage is  $v_{dc}$ . When the armature current goes above  $i_a^* + h$ , the converter is switched such that the armature voltage is  $-v_{dc}$ . Derive an expression for the switching frequency in terms of  $h$ ,  $v_{dc}$ ,  $L_{aa}$ , the voltage constant  $k_v$ , and the rotor speed  $\omega_r$ .

$$i_a < i_a^* - h \quad i_a < i_a^* - h$$

Transistor on

$$v_{dc} = k_v \omega_r + L_{aa} \frac{di_a}{dt}$$

$$\frac{di_a}{dt} = \frac{2h}{T_{on}}$$

$$\Rightarrow L_{aa} \frac{2h}{T_{on}} = v_{dc} - k_v \omega_r \quad \text{or} \quad T_{on} = \frac{2h L_{aa}}{v_{dc} - k_v \omega_r}$$

$$i_a > i_a^* + h$$

Transistor off

$$-v_{dc} = k_v \omega_r + L_{aa} \frac{di_a}{dt}$$

$$\frac{di_a}{dt} = \frac{-2h}{T_{off}}$$

$$\Rightarrow L_{aa} \frac{2h}{T_{off}} = v_{dc} + k_v \omega_r \quad \text{or} \quad T_{off} = \frac{2h L_{aa}}{v_{dc} + k_v \omega_r}$$

$$T_{sw} = T_{on} + T_{off} = 2h L_{aa} \frac{2v_{dc}}{v_{dc}^2 - (k_v \omega_r)^2}$$

$$f_{sw} = \frac{1}{T_{sw}} = \frac{v_{dc}^2 - (k_v \omega_r)^2}{4h L_{aa} v_{dc}} \quad \text{or} \quad \frac{(v_{dc} - k_v \omega_r)(v_{dc} + k_v \omega_r)}{2h L_{aa} v_{dc}}$$