## AAE 439 Hourly Exam \#1 <br> Fall, 2018 Semester

Open Book \& Notes

Attempt all Problems

1. ( 25 pts ) Spinlaunch is one of over 100 small companies supported by venture capital funds to develop small launch vehicles for future orbital constellations of smallsats. Their approach is to reduce launcher size by accelerating the payload and an upper stage propulsion system in a giant centrifuge/catapult to launch the rocket from the Earth's surface at velocities of the order of $5000 \mathrm{mph}(2.2 \mathrm{~km} / \mathrm{s})$. Assume that the firm sets up a launch site at the 28 deg. latitude of Kennedy Space Center and that the upper stage rocket system has an Isp of 300 sec and a propellant mass fraction of $\lambda=0.9$.
i) If the rocket is to place payloads in 150 km circular orbit what is the total $\Delta \mathrm{v}$ that must be imparted by the upper stage system neglecting any gravity, drag or steering losses?
ii) If the desired spacecraft payload has a mass of 100 kg , that what is the gross mass that must be accelerated by the catapult?
iii) The mass fraction of 0.9 is likely ambitious given that the entire system is exposed to high acceleration loads by the catapult. At what $\lambda$ does the entire concept become unviable?
2. (30 pts) The sketch below shows a launch vehicle engine that operates with a chamber pressure of 1200 psi and delivers a c* value of $5000 \mathrm{f} / \mathrm{s}$. Engineers have developed a translating nozzle extension that can be deployed at high altitudes to augment thrust in the latter portions of the boost trajectory. Assuming ideal performance and an average ratio of specific heats of 1.2 for the nozzle flow, determine:
i) Sea level thrust and specific impulse
ii) Vacuum thrust and specific impulse
iii) In order to maximize performance, what altitude should the nozzle extension be deployed?

3. ( 30 pts ) The solid rocket motor shown below is fired at sea level on a test stand. Measured pressure and thrust data are curvefit to give the following results:

$$
\begin{aligned}
& p_{c}=600+63.3 t-1.22 t^{2}, 0 \leq \mathrm{t} \leq 60 \mathrm{sec}, \mathrm{p}_{c} \square \mathrm{psi} \\
& F=6600+696 t-13.4 t^{2}, 0 \leq \mathrm{t} \leq 60 \mathrm{sec}, F \square \mathrm{lbf}
\end{aligned}
$$

The c* value for its propellant is $5000 \mathrm{f} / \mathrm{s}$. Using these data and the motor dimensions in the sketch, determine:
i) The propellant weight in the motor, $\mathrm{m}_{\mathrm{p}}$, in lbf
ii) The sea level specific impulse (in seconds)
iii) The vacuum specific impulse (in seconds)

4. ( 15 pts ) Consider the pros/cons of the Spinlaunch approach described in Problem \#2 \#1. List and briefly discuss three pros and three cons of this approach relative to a conventional two-stage launch vehicle. Specifically address loss mechanisms (gravity, drag, and steering) for this concept in one of your three pros/cons. Are losses greater or less than conventional launch vehicles?

| $\epsilon$ | $M_{e}$ | $p_{e} / p_{c}$ | $C_{f \text {-opt }}$ | $C_{f v}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1.0 | 1.000 | 0.5643080 | 0.67753 | 1.24184 |
| 2.0 | 2.055 | 0.1207748 | 1.22420 | 1.46575 |
| 3.0 | 2.397 | 0.0656052 | 1.35714 | 1.55396 |
| 4.0 | 2.619 | 0.0435133 | 1.43312 | 1.60717 |
| 5.0 | 2.785 | 0.0319051 | 1.48482 | 1.64435 |
| 6.0 | 2.917 | 0.0248603 | 1.52331 | 1.67247 |
| 7.0 | 3.027 | 0.0201796 | 1.55359 | 1.69485 |
| 8.0 | 3.122 | 0.0168690 | 1.57833 | 1.71328 |
| 9.0 | 3.205 | 0.0144174 | 1.59911 | 1.72887 |
| 10.0 | 3.278 | 0.0125373 | 1.61693 | 1.74231 |
| 11.0 | 3.345 | 0.0110547 | 1.63247 | 1.75408 |
| 12.0 | 3.405 | 0.0098591 | 1.64620 | 1.76451 |
| 13.0 | 3.461 | 0.0088767 | 1.65847 | 1.77386 |
| 14.0 | 3.512 | 0.0080569 | 1.66952 | 1.78232 |
| 15.0 | 3.560 | 0.0073636 | 1.67957 | 1.79002 |
| 16.0 | 3.604 | 0.0067703 | 1.68875 | 1.79708 |
| 17.0 | 3.646 | 0.0062577 | 1.69721 | 1.80359 |
| 18.0 | 3.686 | 0.0058107 | 1.70502 | 1.80962 |
| 19.0 | 3.723 | 0.0054180 | 1.71229 | 1.81523 |
| 20.0 | 3.759 | 0.0050705 | 1.71906 | 1.82047 |
| 21.0 | 3.792 | 0.0047611 | 1.72540 | 1.82538 |
| 22.0 | 3.824 | 0.0044840 | 1.73135 | 1.83000 |
| 23.0 | 3.855 | 0.0042346 | 1.73696 | 1.83436 |
| 24.0 | 3.885 | 0.0040091 | 1.74226 | 1.83848 |
| 25.0 | 3.913 | 0.0038043 | 1.74728 | 1.84238 |
| 26.0 | 3.940 | 0.0036175 | 1.75204 | 1.84609 |
| 27.0 | 3.966 | 0.0034467 | 1.75656 | 1.84962 |
| 28.0 | 3.991 | 0.0032898 | 1.76088 | 1.85299 |
| 29.0 | 4.016 | 0.0031453 | 1.76499 | 1.85621 |
| 30.0 | 4.039 | 0.0030119 | 1.76893 | 1.85928 |
| 31.0 | 4.062 | 0.0028883 | 1.77270 | 1.86223 |
| 32.0 | 4.084 | 0.0027735 | 1.77631 | 1.86506 |
| 33.0 | 4.105 | 0.0026667 | 1.77978 | 1.86778 |
| 34.0 | 4.126 | 0.0025671 | 1.78312 | 1.87040 |
| 35.0 | 4.146 | 0.0024740 | 1.78633 | 1.87292 |
| 36.0 | 4.166 | 0.0023868 | 1.78943 | 1.87535 |
| 37.0 | 4.185 | 0.0023050 | 1.79241 | 1.87770 |
| 38.0 | 4.204 | 0.0022281 | 1.79529 | 1.87996 |
| 40.0 | 4.222 | 0.0021557 | 1.79808 | 1.88215 |
|  |  | 0.0020874 | 1.80078 | 1.88427 |


| Thrust Coefficient |
| :--- |
| Ratio of specific heats $=1.2$ |

$$
\mathrm{psl}=14.696 \mathrm{psi}=1.0132 \times 105 \mathrm{~Pa}, \mathrm{Tsl}=518.6 \mathrm{R}=288.16 \mathrm{~K}
$$

$$
\text { rhosl }=0.002377 \mathrm{slug} / \mathrm{f} 3=1.226 \mathrm{~kg} / \mathrm{m} 3, \quad \text { asl }=1116.4 \mathrm{f} / \mathrm{s}=340.0 \mathrm{~m} / \mathrm{s}
$$

| $\mathrm{h}, \mathrm{kft}$ | $\mathrm{h}, \mathrm{km}$ | $\mathrm{p} / \mathrm{psl}$ | rho/rhosl | T/Tsl | a/asl |
| ---: | ---: | :--- | :--- | :---: | :---: |
| -1.0 | -0.305 | 1.0370 | 1.0300 | 1.0069 | 1.0034 |
| 0.0 | 0.000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| 2.0 | 0.610 | 0.9305 | 0.9434 | 0.9862 | 0.9931 |
| 4.0 | 1.219 | 0.8645 | 0.8890 | 0.9725 | 0.9861 |
| 6.0 | 1.829 | 0.8021 | 0.8366 | 0.9587 | 0.9792 |
| 8.0 | 2.438 | 0.7430 | 0.7862 | 0.9450 | 0.9721 |
| 10.0 | 3.048 | 0.6880 | 0.7387 | 0.9313 | 0.9650 |
| 12.0 | 3.658 | 0.6363 | 0.6935 | 0.9175 | 0.9579 |
| 14.0 | 4.267 | 0.5878 | 0.6504 | 0.9038 | 0.9507 |
| 16.0 | 4.877 | 0.5424 | 0.6094 | 0.8901 | 0.9434 |
| 18.0 | 5.486 | 0.4999 | 0.5704 | 0.8763 | 0.9361 |
| 20.0 | 6.096 | 0.4601 | 0.5334 | 0.8626 | 0.9288 |
| 22.0 | 6.706 | 0.4229 | 0.4982 | 0.8489 | 0.9214 |
| 24.0 | 7.315 | 0.3882 | 0.4648 | 0.8352 | 0.9139 |
| 26.0 | 7.925 | 0.3559 | 0.4332 | 0.8214 | 0.9063 |
| 28.0 | 8.534 | 0.3257 | 0.4033 | 0.8077 | 0.8987 |
| 30.0 | 9.144 | 0.2977 | 0.3750 | 0.7940 | 0.8911 |
| 32.0 | 9.754 | 0.2717 | 0.3482 | 0.7803 | 0.8834 |
| 34.0 | 10.363 | 0.2475 | 0.3229 | 0.7666 | 0.8756 |
| 36.0 | 10.973 | 0.2250 | 0.2985 | 0.7540 | 0.8683 |
| 38.0 | 11.582 | 0.2045 | 0.2720 | 0.7519 | 0.8671 |
| 40.0 | 12.192 | 0.1858 | 0.2472 | 0.7519 | 0.8671 |
| 42.0 | 12.802 | 0.1689 | 0.2246 | 0.7519 | 0.8671 |
| 44.0 | 13.411 | 0.1534 | 0.2041 | 0.7519 | 0.8671 |
| 46.0 | 14.021 | 0.1395 | 0.1855 | 0.7519 | 0.8671 |
| 48.0 | 14.630 | 0.1267 | 0.1685 | 0.7519 | 0.8671 |
| 50.0 | 15.240 | 0.1152 | 0.1532 | 0.7519 | 0.8671 |

